YILDIZ TECHNICAL UNIVERSITY NAVAL ARCHITECTURE AND WARITIWE FACULTY DEPARTIVIENT OF NAVAL ARCHITECTURE AND WARINE ENGINEERING BSc. GRADUATE THESIS

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DESIGN OF MOTORYACHT SERIES IN 24M, 21M, 18M



Aims of the Thesis

The decision process in yacht design includes a number of parameters such as yacht type, characteristics, marine conditions, capacity, changing competition and market conditions of the commercial or private working areas preferred by the yacht owner.

The project aims to create a conceptual design by considering these parameters.

Calculations and Plans for Reference (24 M Motor Yacht)

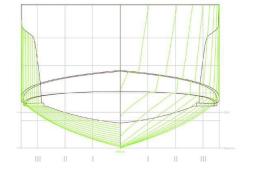


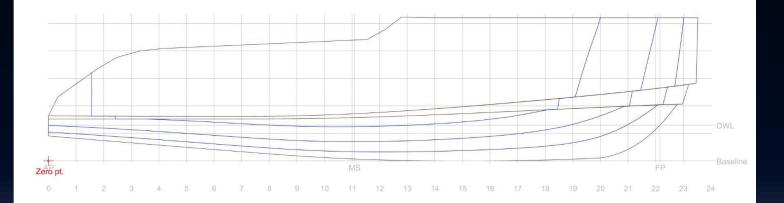


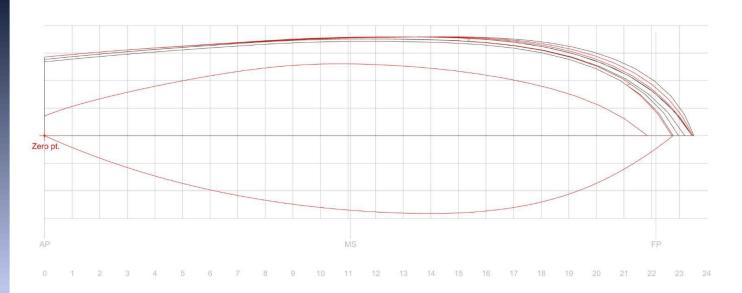


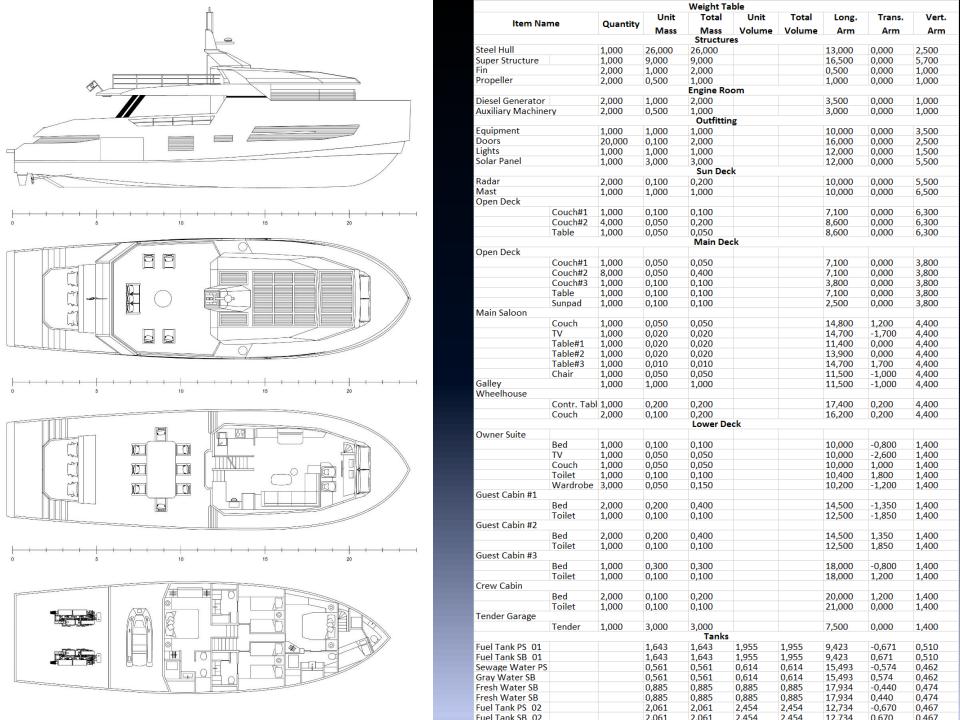


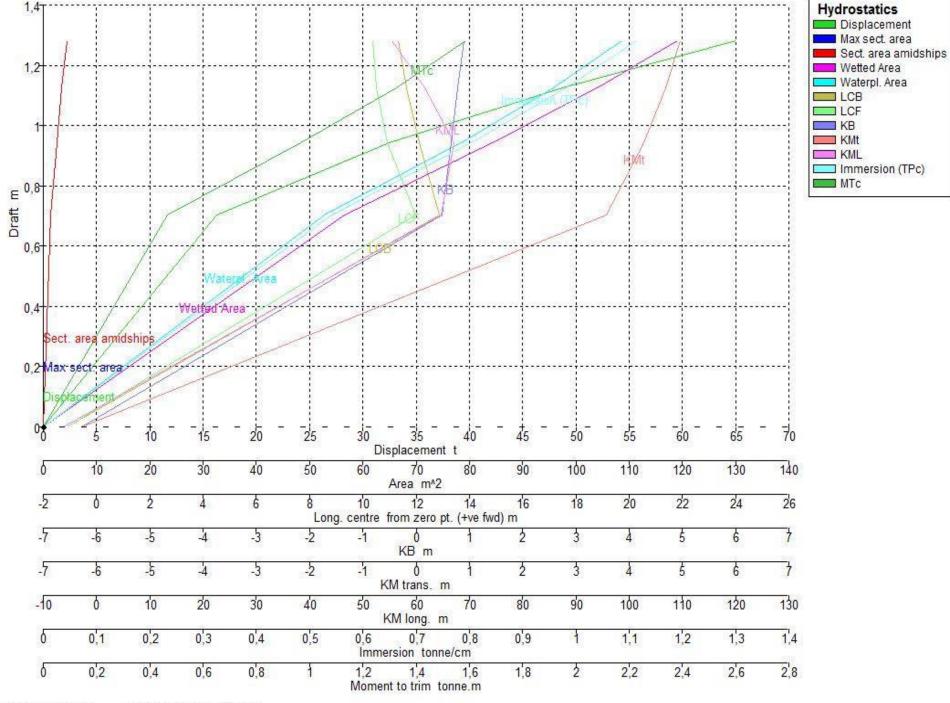




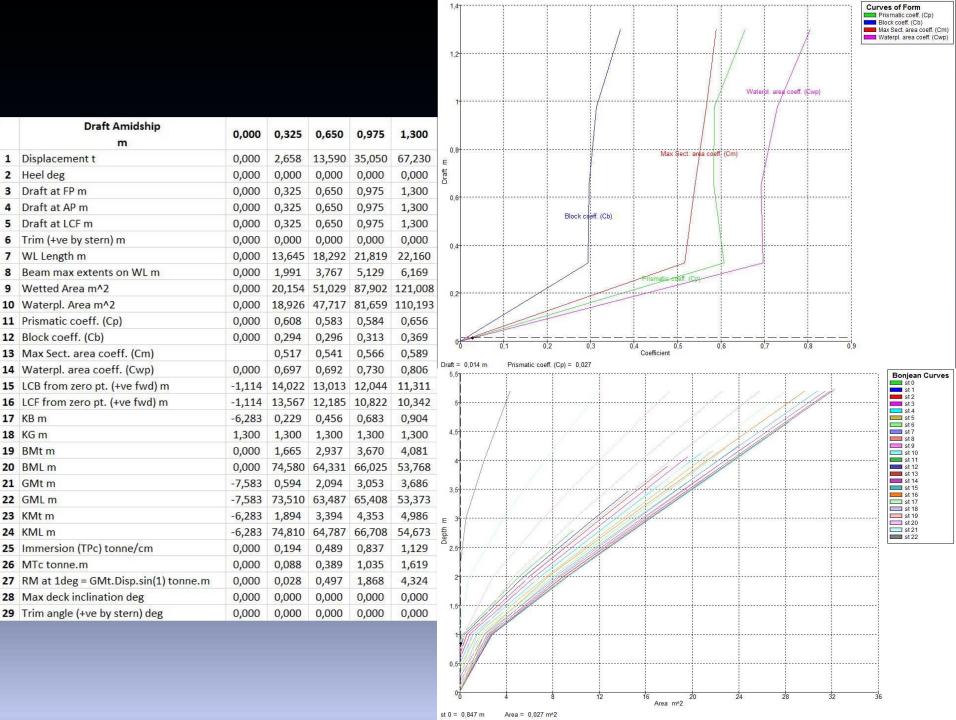


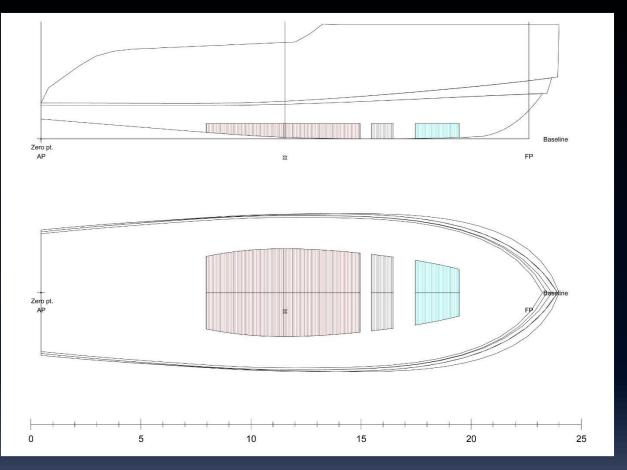






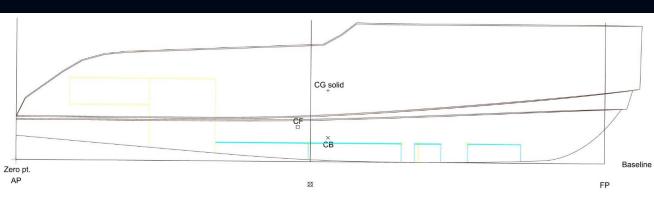
Draft = 0.000 m Displacement = 0.000 t





| Tank Name | Total Mass tonne | Total Volume m^3 | Specific Gravity | Fluid Type | Long. Arm m | Trans. Arm | Vert. Arm m |
|-----------------|---------------------|------------------------|---------------------|-------------|----------------|------------|----------------|
| Fuel Tank PS_01 | 1,643 | 1,955 | 0,84 | Diesel | 9,423 | -0,671 | 0,51 |
| Fuel Tank SB_01 | 1,643 | 1,955 | 0,84 | Diesel | 9,423 | 0,671 | 0,51 |
| Fuel Tank PS_02 | 2,061 | 0,614 | 0,84 | Diesel | 15,493 | -0,574 | 0,462 |
| Fuel Tank SB_02 | 2,061 | 0,614 | 0,84 | Diesel | 15,493 | 0,574 | 0,462 |
| Sewage Water PS | 0,561 | 0,885 | 0,913 | Slops | 17,934 | -0,44 | 0,474 |
| Gray Water SB | 0,561 | 0,885 | 0,913 | Slops | 17,934 | 0,44 | 0,474 |
| Fresh Water SB | 0,885 | 2,454 | 1 | Fresh Water | 12,734 | -0,67 | 0,467 |
| Fresh Water SB | 0,885 | 2,454 | 1 | Fresh Water | 12,734 | 0,67 | 0,467 |

Loadcase 1 – Departure (Fuels, Fresh Water Full)

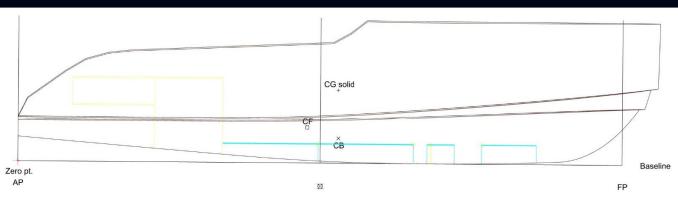


Disp:66.20 t, Tamid: 1,295 m, Trim: -0,144 m, Heel: -0,4 deg (stbd)

| | | Loadcase - Departure | |
|---|----|--------------------------------------|-------|
| | 1 | Draft Amidships m | 1,306 |
| | 2 | Displacement t | 67,32 |
| | 3 | Heel deg | -0,4 |
| l | 4 | Draft at FP m | 1,395 |
| l | 5 | Draft at AP m | 1,216 |
| l | 6 | Draft at LCF m | 1,302 |
| l | 7 | Trim (+ve by stern) m | -0,18 |
| | 8 | WL Length m | 22,25 |
| | 9 | Beam max extents on WL m | 6,176 |
| | 10 | Wetted Area m^2 | 120,3 |
| | 11 | Waterpl. Area m^2 | 109,6 |
| | 12 | Prismatic coeff. (Cp) | 0,644 |
| | 13 | Block coeff. (Cb) | 0,356 |
| | 14 | Max Sect. area coeff. (Cm) | 0,585 |
| | 15 | Waterpl. area coeff. (Cwp) | 0,797 |
| | 16 | LCB from zero pt. (+ve fwd) m | 11,74 |
| | 17 | LCF from zero pt. (+ve fwd) m | 10,6 |
| | 18 | KB m | 0,907 |
| | 19 | KG solid m | 2,682 |
| | 20 | BMt m | 4,003 |
| | 21 | BML m | 53,16 |
| l | 22 | GMt corrected m | 2,228 |
| l | 23 | GML m | 51,39 |
| l | 24 | KMt m | 4,91 |
| l | 25 | KML m | 54,07 |
| l | 26 | Immersion (TPc) tonne/cm | 1,123 |
| | 27 | MTc tonne.m | 1,561 |
| | 28 | RM at 1deg = GMt.Disp.sin(1) tonne.m | 2,618 |
| | 29 | Max deck inclination deg | 0,584 |
| | 30 | Trim angle (+ve by stern) deg | -0,46 |



Loadcase 2 – Arrival (Gray Water, Black Water Full)

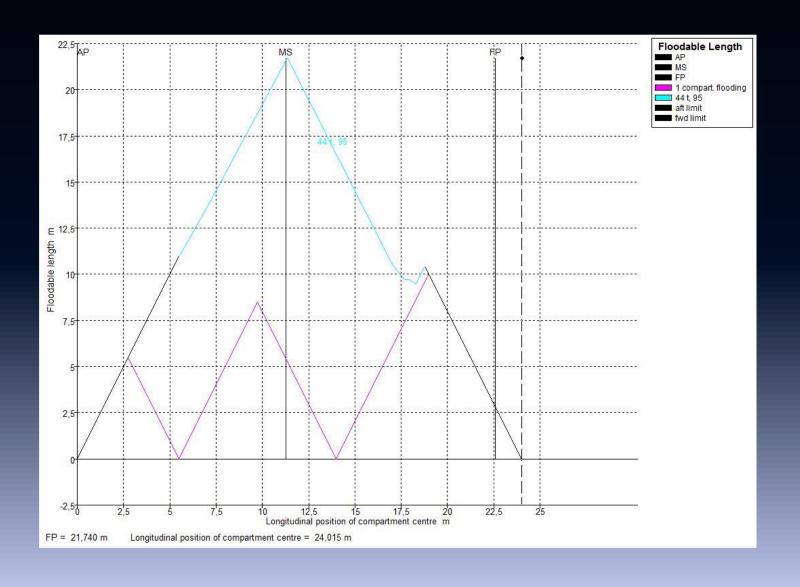


Disp:58.14 t, Tamid: 1,219 m, Trim: -0,056 m, Heel: -0,5 deg (stbd)

| | Loadcase - Arrival | |
|----|--------------------------------------|-------|
| 1 | Draft Amidships m | 1,306 |
| 2 | Displacement t | 67,32 |
| 3 | Heel deg | -0,4 |
| 4 | Draft at FP m | 1,395 |
| 5 | Draft at AP m | 1,216 |
| 6 | Draft at LCF m | 1,302 |
| 7 | Trim (+ve by stern) m | -0,18 |
| 8 | WL Length m | 22,25 |
| 9 | Beam max extents on WL m | 6,176 |
| 10 | Wetted Area m^2 | 120,3 |
| 11 | Waterpl. Area m^2 | 109,6 |
| 12 | Prismatic coeff. (Cp) | 0,644 |
| 13 | Block coeff. (Cb) | 0,356 |
| 14 | Max Sect. area coeff. (Cm) | 0,585 |
| 15 | Waterpl. area coeff. (Cwp) | 0,797 |
| 16 | LCB from zero pt. (+ve fwd) m | 11,74 |
| 17 | LCF from zero pt. (+ve fwd) m | 10,6 |
| 18 | KB m | 0,907 |
| 19 | KG solid m | 2,682 |
| 20 | BMt m | 4,003 |
| 21 | BML m | 53,16 |
| 22 | GMt corrected m | 2,228 |
| 23 | GML m | 51,39 |
| 24 | KMt m | 4,91 |
| 25 | KML m | 54,07 |
| 26 | Immersion (TPc) tonne/cm | 1,123 |
| 27 | MTc tonne.m | 1,561 |
| 28 | RM at 1deg = GMt.Disp.sin(1) tonne.m | 2,618 |
| 29 | Max deck inclination deg | 0,584 |
| 30 | Trim angle (+ve by stern) deg | -0,46 |

| | C | 3.1 | ı 1.2.4: Initial | GMt GM | 1 at 0,0 de | eg = 1,79 | 9 m | | | | | | | | 3.1.2.4: Ini 3.1.2.5: Pa 3.1.2.6: Tu 3.2.2: Sev 3.2.2: Sev | assenger Irn: angle ere wind a ere wind a | crowding: of equilib and rolling and rolling | angle of rium Wind He Wind He | equilibriu eling (ste | ady) | | | | |
|--------|---|------------|---|----------------|-------------|---------------------|-----------------|---------------------------|-------------|---|------------------------|--|--------|------------------------|--|--|---|--|---|---------------------|-------------|---|-----------|--------------|
| | | | ì | | M | x GZ = | | at 44,5 de | | and tollin | na Wind H | laolina (a | uret) | | Max GZ = I | 0,654 m a | t 44,5 deg | J. | 0.000 | | | | | |
| | |),6 | 1 / | | | 322 | 1 | 3.2.2. Sev | | | | senud 15 | NSUII. | | | | | | | | | | | |
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| | | | V 3.1.2.5 | : Passe | nger craw | ප්ථාරු නි ගල | te efieteu | i dibeniumi li bri | um | | | | | | | | | | | | | | | |
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| | 21 | 1,5 |) | | | <u> </u> | | | | | | | | | | | | | | | | | | |
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| | F1 | ,8 -25 | b . | 25 | į | 0 | 75 | | 00 | 125 | 1 | 50 | 175 | | | | | | | | | | | |
| | G7 = | 0,017 m | Heel to St | arboard | = 0.000 | | Starboa | ra aeg. from zero | hool) = | U U3U34 | m dea | | | | | | | | | | | | | |
| | Heel to Starboard deg | 0,017 111 | -30,0 | | | 0,0 | 10,0 | | 30,0 | 40,0 | 50,0 | 60,0 | 70,0 | 80,0 | 90,0 | 100,0 | 110,0 | 120,0 | 130,0 | 140,0 | 150,0 | 160,0 | 170,0 | 180,0 |
| | GZ m | | 05000000000 | -0,51 | | Description 1 | | 0,545 | 0.01.050.00 | 120000000000000000000000000000000000000 | 10000180101- | | | 0.554.700 | | | | | | | | | -1,16 | |
| 2 | Area under GZ curve from zero | heel m.deg | 11,29 | 5,65 | 1,467 | 0,03 | 1,799 | 6,298 | 12,26 | 18,7 | 25,22 | 31,51 | 37,18 | 41,43 | 43,27 | 42,18 | 37,97 | 30,68 | 20,62 | 8,166 | -6,2 | -21,5 | -35,5 | -41,9 |
| 3 | Displacement t | | 58,14 | 58,14 | 58,14 | 58,15 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 | 58,14 |
| 4 | Draft at FP m | | 0,889 | 1,091 | 1,211 | 1,247 | 1,211 | 1,091 | 0,889 | 0,582 | 0,08 | -0,95 | -3,27 | -10,3 | n/a | -17,7 | -10,6 | -8,2 | -6,99 | -6,26 | -5,78 | -5,44 | -5,25 | -5,2 |
| 5 | Draft at AP m | | 0,52 | 0,861 | 1,091 | 1,191 | 1,091 | 0,861 | 0,52 | 0,012 | -0,78 | -2,08 | -4,58 | -11,7 | n/a | -16 | -8,83 | -6,36 | -5,06 | -4,26 | -3,73 | -3,37 | -3,18 | -3,16 |
| | WL Length m | | 200000000000000000000000000000000000000 | A COLUMN TOWNS | 22,07 | 30003-00-000 | 198030118 13001 | 550500 E100000 | | 1777-1036 - 177-1 | 2555.00 * 30350 | The state of the s | 100000 | 30/300 * 000000 | 1860A-CO* 17700000 | 100,000 Pt. 2000.00 | 700 700 00 Page 1500 00 | 75.055.07 * 733393345 | 200 00000000000000000000000000000000000 | A C. Dillo. Replace | | 1 1000 Per 101-100 | 100000000 | 110000 |
| 7 | Beam max extents on WL m | | 5,083 | 5,322 | 5,828 | 5,932 | 5,828 | 5,322 | 5,083 | 5,099 | 5,205 | 5,236 | 4,975 | 4,542 | 4,278 | 4,143 | 4,118 | 4,201 | 4,341 | 4,386 | 4,768 | 5,733 | 7,289 | 7,179 |
| 1.0000 | Wetted Area m^2 | | 100000000000000000000000000000000000000 | | 113,8 | | | | | | | | | | 98,16 | 500000 * 110000 * | ************************************** | V | | | 190,000,000 | 13.00.000.000.000 | 131,9 | 10.000.00.00 |
| 2-779 | Waterpl. Area m^2 | | | | 103,1 | | | | | | | | | | | | | | | | | | | |
| 200000 | Prismatic coeff. (Cp) | | | | 0,636 | | | | | | | | | | | | | | | | | | | |
| | Block coeff. (Cb) | | 100 | | 0,381 | | | | | | | | | | | | | | | | | | | |
| 2000 | LCB from zero pt. (+ve fwd) m | | | | 11,61 | | | | | | | | | | | | | | | | | | | |
| | LCF from zero pt. (+ve fwd) m | | 11,21 | | 10,55 | | | | | | | | | | 11,57 | | | | | | | | | |
| - | Max deck inclination deg Trim angle (+ve by stern) deg | | 30,01 | | -0,31 | 0,145 | | 20,01 | | | | | 70 | | | | | | 110000000000000000000000000000000000000 | 1-10-0-1 | | 15.000000000000000000000000000000000000 | 168,7 | 100000 00000 |

Floodable Length Graph and Bulkhead Locations

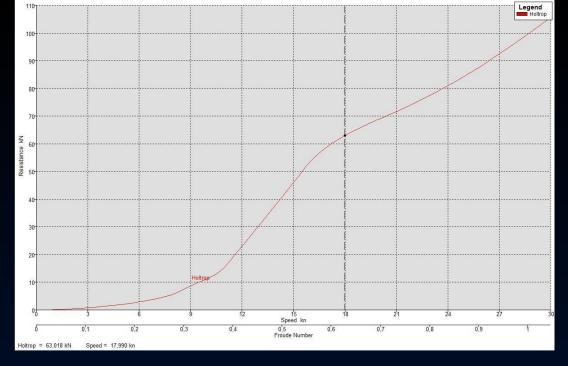


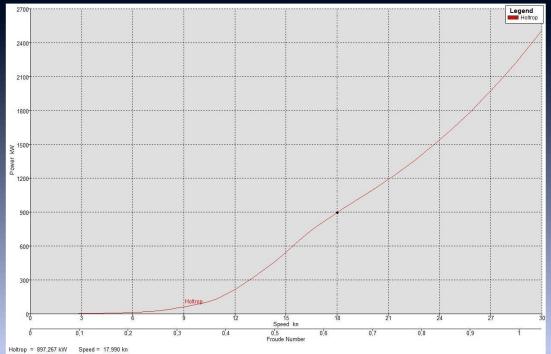
IMO Criteria

| | IMO CRITERIA | | | | | |
|--|---|--------|-------|---------|------|---------|
| | 3.1.2.1: Area 0 to 30 | | | Pass | | |
| | from the greater of | | | | | |
| A 740/49) Ch2 Davies situation | spec. heel angle | 0 | deg | 0 | | |
| A.749(18) Ch3 - Design criteria applicable to all ships | to the lesser of | | | | | |
| applicable to all ships | spec. heel angle | 30 | deg | 30 | | |
| | angle of vanishing stability | 102 | deg | | | |
| | shall not be less than (>=) | 3,1513 | m.deg | 14,6733 | Pass | 365,63 |
| | 3.1.2.1: Area 0 to 40 | | | | Pass | |
| | from the greater of | | | | | |
| | spec. heel angle | 0 | deg | 0 | | |
| A.749(18) Ch3 - Design criteria | | | | | | |
| applicable to all ships | spec. heel angle | 40 | deg | 40 | | |
| | first downflooding angle | n/a | deg | | | |
| | angle of vanishing stability | 102 | deg | | | |
| | shall not be less than (>=) | 5,1566 | m.deg | 22,7816 | Pass | 341,79 |
| | 3.1.2.1: Area 30 to 40 | | | | Pass | |
| | from the greater of | | | | | |
| | spec. heel angle | 30 | deg | 30 | | |
| A.749(18) Ch3 - Design criteria | to the lesser of | | | | | |
| applicable to all ships | spec. heel angle | 40 | deg | 40 | | |
| | first downflooding angle | n/a | deg | | | |
| | angle of vanishing stability | 102 | deg | | | |
| | shall not be less than (>=) | 1,7189 | m.deg | 8,1083 | Pass | 371,71 |
| | 3.1.2.2: Max GZ at 30 or greater | | | | Pass | |
| | in the range from the greater of | | | | | |
| | spec. heel angle | 30 | deg | 30 | | |
| A.749(18) Ch3 - Design criteria | to the lesser of | | | | | |
| applicable to all ships | spec. heel angle | 90 | deg | | | |
| applicable to all ships | angle of max. GZ | 59,1 | deg | 59,1 | | |
| | shall not be less than (>=) | 0,2 | m | 0,912 | Pass | 356 |
| | Intermediate values | | | | | |
| | angle at which this GZ occurs | | deg | 59,1 | | |
| A.749(18) Ch3 - Design criteria | 3.1.2.3: Angle of maximum GZ | | | | Pass | |
| applicable to all ships | shall not be less than (>=) | 25 | deg | 59,1 | Pass | 136,36 |
| A.749(18) Ch3 - Design criteria | 3.1.2.4: Initial GMt | | | | Pass | |
| applicable to all ships | spec, heel angle | 0 | deg | | | |
| applicable to all ships | shall not be less than (>=) | 0,15 | m | 2,228 | Pass | 1385,33 |
| | 3.1.2.5: Passenger crowding: angle of equilibrium | | | | Pass | |
| | Pass. crowding arm = nPass M / disp. D cos^n(phi) | | | | | |
| | number of passengers: nPass = | 0 | | | | |
| A.749(18) Ch3 - Design criteria | passenger mass: M = | 0,075 | tonne | | | |
| applicable to all ships | distance from centre line: D = | 0 | m | | | |
| applicable to all ships | cosine power: n = | 0 | | | | |
| | shall not be greater than (<=) | 10 | deg | -0,4 | Pass | 103,51 |
| | Intermediate values | | | | | |
| | Heel arm amplitude | | m | 0 | | |
| | 3.1.2.6: Turn: angle of equilibrium | | | | Pass | |
| | Turn arm: a v^2 / (R g) h cos^n(phi) | | | | | |
| | constant: a = | 0,9996 | | | | |
| | vessel speed: v = | 0 | kn | | | |
| | turn radius, R, as percentage of Lwl | 510 | | | | |
| applicable to all ships | h = KG - mean draft / 2 | 2,029 | m | | | |
| | cosine power: n = | 0 | | | | |
| | shall not be greater than (<=) | 10 | deg | -0,4 | Pass | 103,51 |
| | Intermediate values | | | | | |
| | Heel arm amplitude | | m | 0 | | |

Resistance – Speed Graph

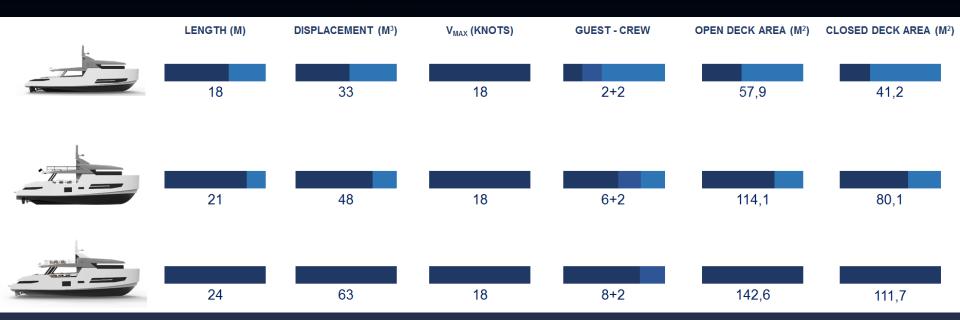
Power – Speed Graph





SUMMARY

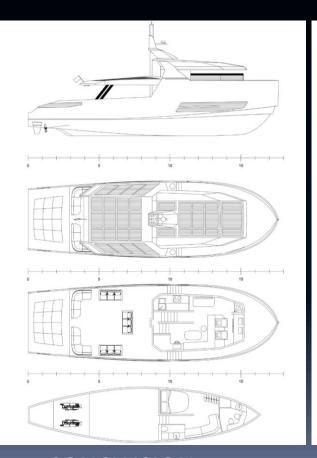
Comparision about main properties of 24 M, 21 M, 18 M

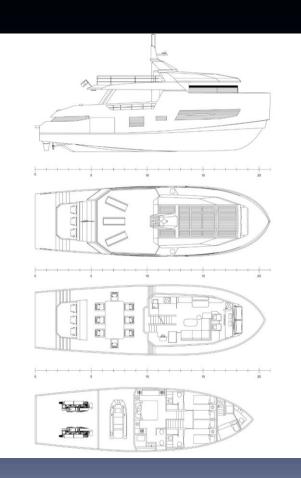


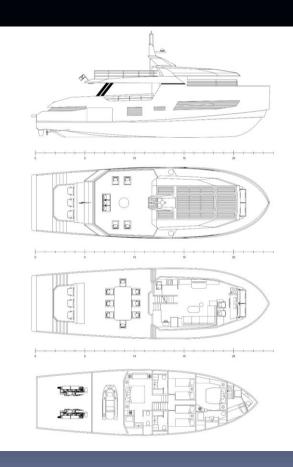
CONCLUSION

Boats of different sizes but with the same concept are designed for different budgets. In order to be preferable in terms of ergonomics and economics, the general layout of the 24 m motor yacht, which is taken as a reference, has been rearranged for 21 meters and 18 meters. A good step has been taken for the accessibility of motoryachts, one of the main objectives.

Comparision Between GA's

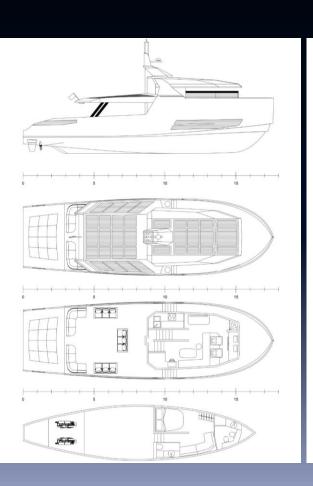


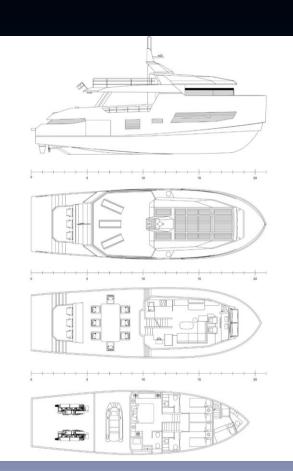


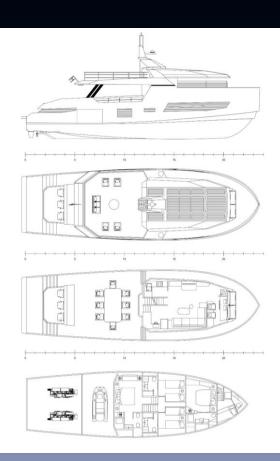


CONCLUSION

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Thanks For Listening